The properties of glass lining
Elementary ingredients for technical Düker enamels

The ultimate hardness. Based on fire, water, air and earth…

It takes very little to ensure that production processes in sensitive industrial areas are carried out safely: quartz, feldspar, borax, sodium carbonate, salt petre and metal oxides are processed in several stages to become technical enamel. The special mixing proportions of the basic substances determine the final resistance of the end product to aggressive media.

Technical enamel is therefore a very special surface protection and its uses include the chemical, pharmaceutical and food industries. It meets quality and economic requirements in that components made of email800 reduce the usual amount of care and maintenance required. Düker pipelines, fittings, valves, bottom outlet valves and columns can be combined to form durable complex units. The many options for users include the standard range, the design of special parts or a customised combination of both.

The characteristics of our glass lining

Chemical resistance

New products and new process techniques are creating larger areas of use and more exacting requirements for surface protection in plant engineering. We catered for these requirements when developing our “Glass Lining Technologies” particularly durable email800 and glass lining which are different with regard to technical specifications like email250 and email850P.

email800 is highly resistant against attack, wear and corrosion and against diffusion during long holding times. These characteristics have been confirmed by independent tests and major chemical laboratories in Germany and Switzerland. Here are some data:

Acid Resistance:
- will be checked according to chapter 12 of DIN EN ISO 28706-2 - boiling acid

Alkali Resistance:
- will be checked according to chapter 9 of DIN EN ISO 28706-4 - alkaline fluidity

Corrosion velocity in NaOH-aqueous solutions

![Corrosion velocity in NaOH-aqueous solutions graph]

Corrosion velocity in HCL-aqueous solutions

![Corrosion velocity in HCL-aqueous solutions graph]

Corrosion velocity in H$_2$SO$_4$-aqueous solutions

![Corrosion velocity in H$_2$SO$_4$-aqueous solutions graph]
The properties of our glass lining

Physical properties

Thermal shock resistance

The thermal shock resistance of glass lining is mainly determined by the prestress of the glass. Düker email800 has a prestress on the steel of about 120 N/mm² at room temperature. This is achieved by adjusting the expansion coefficient. When temperature increases the prestress decreases until it disappears at about 350 °C (see stress curve).

The table of the thermal shock resistance of glass lined parts considers this reduction. Furthermore it takes into account that the most danger to the hot glass is when subjected to cold product. Exceeding the permissible temperatures can result in tearing and later on in cracking of the enamel on the pipewall.

<table>
<thead>
<tr>
<th>Material data:</th>
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<tbody>
<tr>
<td>• Specific weight 2.5 g/cm³</td>
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<tr>
<td>• Coefficient of thermal conductivity 1.2 W/mK</td>
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<tr>
<td>• Modulus of elasticity 80,000 N/mm²</td>
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<tr>
<td>• Compressive strength -800 N/mm²</td>
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<tr>
<td>• Tensile strength 80 N/mm²</td>
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<tr>
<td>• Dielectric strength 20-30 kV/mm</td>
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<tr>
<td>• Surface finish of enamel 0.05 µm</td>
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</table>

Stress curve in the enamel of steel

Application examples

We use the temperature of the enamelled pipewall (TW) as the basis. At a given temperature TW (°C) the temperature of the product should be between T₁ and T₂ and the temperature of the heating/cooling agent should be between T₃ and T₄.

1. Hot product
The temperature of the pipewall is 50 °C. Which temperature must be exceeded?
From TW = 50 °C horizontal in the table to T₁ = 180 °C

2. Cold product
The temperature of the pipewall is 290 °C. Which temperature must the product have at least?
From TW = 200 °C horizontal to T₂ = 100 °C

3. Heating
The temperature of the pipewall is 20 °C. Which temperature of the heating agent must not be exceeded?
From TW = 20 °C horizontal to T₃ = 150 °C

4. Cooling
The temperature of the pipewall is 180 °C. Which temperature of the cooling agent must not be fallen below?
From TW = 180 °C horizontal to T₄ = 50 °C
Industrial enamel

Industrial enamel as allround material is firmly established between surface finishing materials fulfilling rather inferior demands and the special materials with to some extent very specific performance data particularly in the chemical and pharmaceutical industry but also for water supply systems and in special niches in general machine construction.

Depending upon the area of application enamel with its generally broad function profile can be adjusted to meet special demands. Whether for supplying potable water, textile chemicals or in the treatment of waste water, in soldering plant construction and in the pharmaceutical industry under GMP conditions or to comply with hygienic design stipulations, enamel fulfils many and varied demands with different focal points by linking the structure material with the surface finish determining grades of enamel.

Typical material properties

The term industrial enamel can be seen to be analogue with industrial ceramic. It would appear sensible to differentiate between commercial enamel for every day use in the home or for jewellery, etc., because as far as industrial enamel is concerned the technological demands put on the surface finish are in the foreground. As a consequence, this term is applied for enamelling in processes in which physical and chemical stress conditions can be defined and to comply with hygienic design stipulations, enamel fulfils many and varied demands with different focal points by linking the structure material with the surface finish determining grades of enamel.

The main typical material features of industrial enamel:

- High resistance against corrosion attack, more especially in the case of acidic media even at higher processing temperatures
- Higher resistance against wear by abrasive media
- Surface smoothness (Fig. 1)
- Easy to clean with no tendency towards adhesion
- Biological and catalytic inert behaviour

The properties of the enamel are supported by appropriate sophisticated constructive designs which strengthen the positive properties and overcome existing limitations as far as possible.

Physiochemical compound material

Enamel as such is outstanding when compared with other popular surface coatings and finishes such as wet paint, powder coating, lining with plastic, etc., inter alia by the given intensive physical and chemical connection with the basic material. This is marked by diffusion processes from the basic material towards the enamel and vice versa. Over and above this forms a real compounding layer of but a few but also to some tens of micrometers thick depending on the material system (Fig. 2).

Optimal morphology by releasing elements close to the surface and linking the substrate material in the enamel matrix is initially generated to develop the mechanical and physical connection.

The increased roughness by releasing the substrate surface in connection with the development of backcuts offers a large number of anchor points for micromechanical positive connection.

This mechanism is supplemented by generating integral pressure tension in the enamel in cooled state which contributes in the further stabilisation of the mechanical compound.

However, if the stress in the enamel layer is too high, this can also lead to increased sensitivity towards impact where convex surface elements are concerned.

Enlargement of the specific surface supports the development of intermolecular bonding apart from this mechanical and physical bonding mechanism. Considerable effects are achieved through Valenz and Van-der-Waals bonding but nevertheless, metallic bonding in the bonding layer likewise plays a role in the iron-silicium-oxygen system.

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Fig. 1: Industrial enamel with extremely smooth surface finish in conjunction with high wear resistance to abrasive acting media and high resistance to corrosion. Visual scatter light inspection of surface.

Fig. 2: Detail photograph of a compound layer enamel (in this case with grey cast iron (GGG) electron raster microscope photograph of Fraunhofer Institute ISC, Würzburg) in approx. 5000-fold magnification. Clearly visible is the (micro) roughness of the surface (bright to the bottom) with back cuts. Following to the top is a thinner homogeneous appearing seam about 2µm thick and the actual bonding layer afterwards clearly over 10 µm thick with different precipitations (ferrotitanium crystal in needle and pellet form) and inclusions.
The durability of high acid resistant enamel as used in chemical plant construction, for example, is marked to some extent by extremely high SiO₂-content in compound with titanium, zirconium, lithium and boron. Special modifications are possible if the resistance to lye has to be increased.

Although in theory enamel is considered not to be stable in the case of watery solutions the wear is usually so low that it can be assumed that the technical stability of the system is given but this is not the case with phosphoric and fluoride acid.

For example, the wear rate for 20% HCl at 110 °C is 50 µm per year (equivalent to 9000 working hours). This is to be compared with the typical coat thickness of surface enamel of about 1000 µm. As a rule the respective wear down in the fluid phase is in a t² relationship (t = time).

The quality of any enamel depends on a large number of pertinent parameters and periphery conditions. Of decisive significance is the metallurgical quality of the basic material, its microstructure the mechanical pre-treatment it has been subject to and its surface finish.

Only steels with restricted analysis can be given a high quality enamel finish. Carbon, sulphur and almost all metal accompanying elements must be limited. Clean ferritic microstructure in the periphery layer facilitates enamelling. Carbon inclusions make enamelling more difficult in the same way as micro faults which can act like hydrogen traps. This applies generally for enamelling iron foundry materials.

Thermal and mechanical preparation is subject to two main conditions. Clean, abrasive acting blasting material cleans, activates and enlarges the surface (Fig. 3). However, any contamination of the surface must be avoided after blasting. From this one can see the demand for a very quick production sequence, i.e. pre-treatment, application of the enamel slick, drying and firing the enamel.

The various components have a different effect on both the dissolving behaviour of the oxide coating and the viscosity of the melt. Iron oxide escapes in the over saturated enamel melt and leads to faults that cannot be repaired (such as copper heads, and burn through) should the absorpabilty of the enamel be over stressed as a result of too long or too hot firing. Faults can occur which are also restricted locally in the case of less uniform distribution of the enamel mass.

Apart from the traditional areas of application in chemical plant construction, enamelling is a first choice material system in all those applications where marked resistance towards aggressive media is to be assured in conjunction with the mechanical strength even in the case of high process temperatures.

Fig. 3: Detail photograph of a corundum-blasted steel surface, approx. 3000-fold magnification (scanning electron microscope photograph Fraunhofer-Institut ISC, Würzburg). The surface as a result of the blasting operation is clearly split and eroded. This finish offers an ideal surface for building up the material compound in the subsequent enamelling process.

Fig. 4: Components in front of the furnace after completion of the firing operation. Homogeneous temperature distribution within the component is the basic requirement to ensure quality enamelling.

Apart from the traditional areas of application in chemical plant construction, pharmaceutical and water supply systems, industrial enamelling is gaining increasing significance in general plant and machine construction. Industrial enamelling is a first choice material system in all those applications where marked resistance towards aggressive media is to be assured in conjunction with the mechanical strength even in the case of high process temperatures.

The described sequences and effects contribute to differences in the base enamel (initial or first and second layer on the component) and the top enamel layer (and the build up of the following layer is aimed at ensuring the overall layer thickness).
Mechanical material behavior in composites

Seen from a material science point of view, the enameling process itself can be clearly described and controlled. The physical and chemical interrelationships are known and in general offer a wide scope of possibilities for aligning the interaction between the base material and enamel to determine the surface that provides the best solution for the load conditions present. The mechanical limits of the material system are known and reliably calculable. Any likely fears of the possibility of “spontaneous blistering” are to be attributed to a lack of knowledge of the overall context.

Mechanical material behavior

The use of enameled components has its limits in plant and engine construction where a failure of the material compound of steel or iron with enamel becomes likely. But in many cases the use of enameled components is out of the question from the beginning which is due to a lack or insufficient knowledge of the interrelationships of the materials when it comes to enamelled construction elements.

In addition to other test parameters, the quality of an enameled product can be described by its color coating as well as its adhesive strength and impact resistance on the substrate material. High scores signify a very good material compound and, as a consequence, a high mechanical load capacity.

The dimensions of plant components are usually laid out versus the yield point or 0.2% of yield strength of the construction material, also taking the given safety values into consideration. This method allows a reduced and localized plastic flow for typical materials with a pronounced ductility, in order to reduce local stress peaks.

The construction of enameled construction parts cannot draw on the methods of plant and engine construction where a failure of the material compound or, in other words, the flaking off of the enamel. A purely elastic deformation of the substrate material, however, does have not damaging effect on the enamel layer.

Laboratory samples, results, evaluation

The above mentioned interrelationships were tested and evaluated in a series of tests in co-operation with InfraServ GmbH, Frankfurt, Germany simulating real-life situations. The tests were initially to determine the stress-strain curve of

- smooth pipe samples (DN 15) with an outer enameled surface and
- non-enameled reference samples

during a tensile test (according to test standard EN 10002). The tensile tests were carried out in a saline solution with tension applied between the base material of the sample and a point contact in electrolytes. The damaged enamel was detected visually and by way of the current flow between the sample and point contact.

In addition, tin samples with an enamel layer on one side where tested in a three-point flexural test. The test temperatures were room temperature and 200 °C respectively. The test allows the following basic conclusions to be deduced:

- Failure-free deformation of the entire sample in the elastic area of the stress-strain curve
- Initial failure of the enamel upon reaching the yield point, approx. 250 N/mm²
- Strain-induced failure at the Lüders band of the base material
- Hardening of the base material following the entire delamination of the enamel

Constrution component tests, results, evaluation

Original construction components – pipe endings connected by loose flanges DN 50 as used in the construction of chemical plants – were also tested under tensile and bending load until the point of failure. Regardless of the stress type, this test has also revealed typical failure patterns which correspond to theoretical methods and the laboratory tests carried out.

- The tensile tests result in a tilting of the flange faces beginning at the outside perimeter (reverse flanges) when overload occurs. This kind of plastic deformation leads to a local failure of the enamel in the area of excess load.
- The three-point flexural test reveals localized plastic deformations in the area of the application of force and the points of support. Here, too, and only here, the enamel layer fails and the enamel flakes off.

Conclusion

With regard to the usual engineering design of construction elements which possess a considerable reliability regarding plastic deformation, no restriction as a result of deformation can be initially ascertained with regard to the use of enameled components. Only in the case of impermissible localized plastic deformation, the enamel suffers strain-induced damage.
GLASS LINING TECHNOLOGIES

JOBBING FOUNDRY
FITTINGS AND VALVES
DRAINAGE TECHNOLOGY
ENGINEERING

04.05.2015 Specifications subject to change without notice.